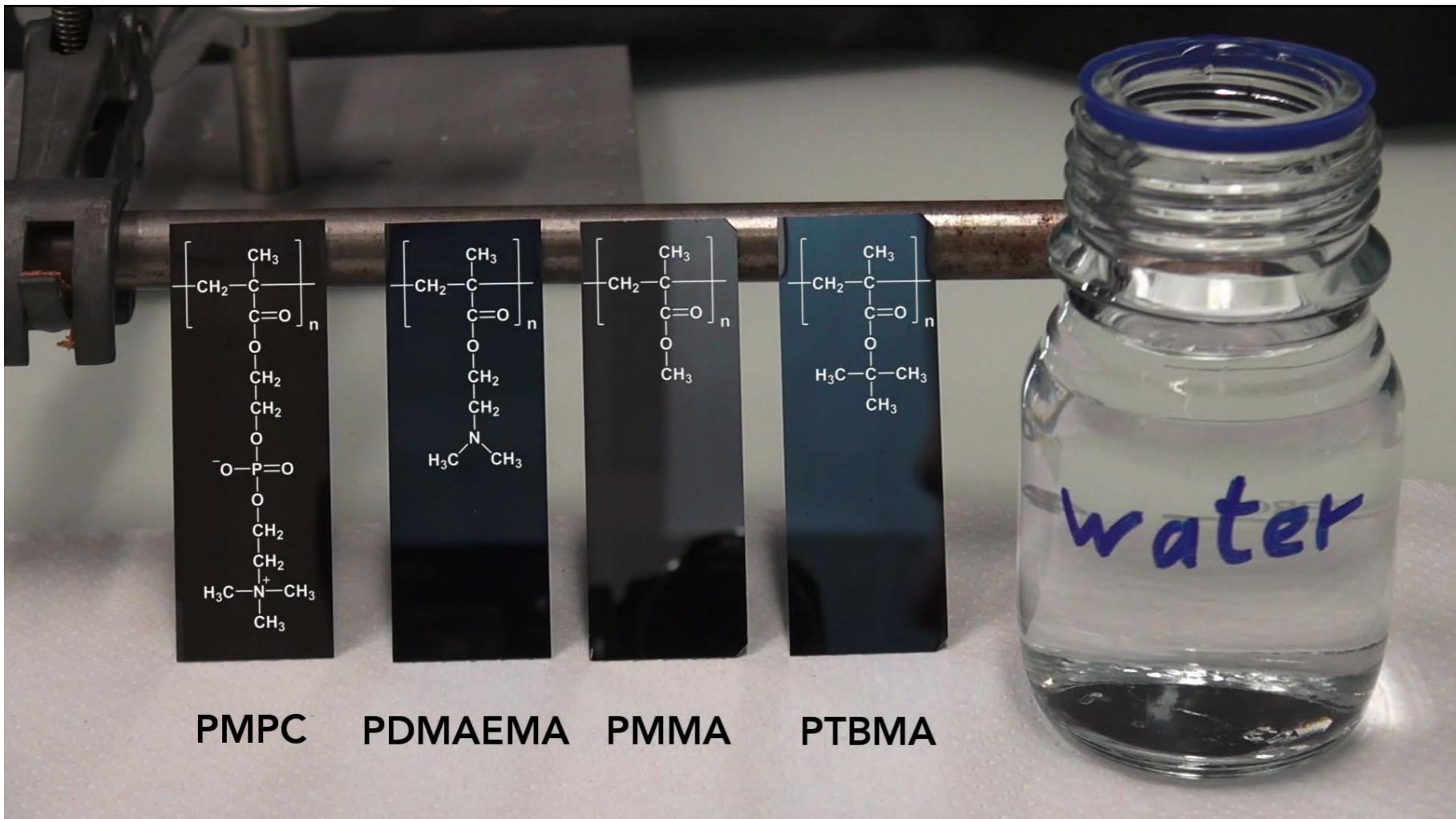


Course: Physical Chemistry of Polymeric Materials

Surfaces and Interfaces: Characterization of the Wettability of Solid Surfaces

Surface Wetting



PMPC

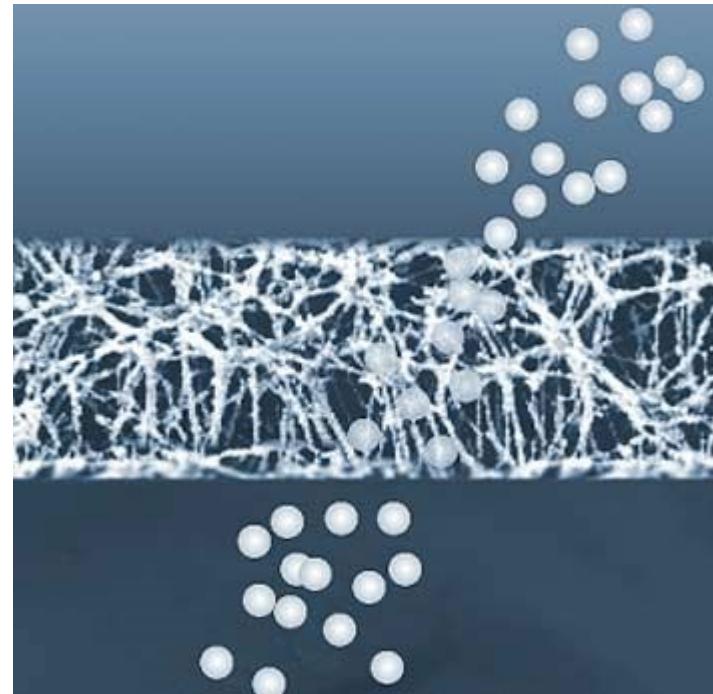
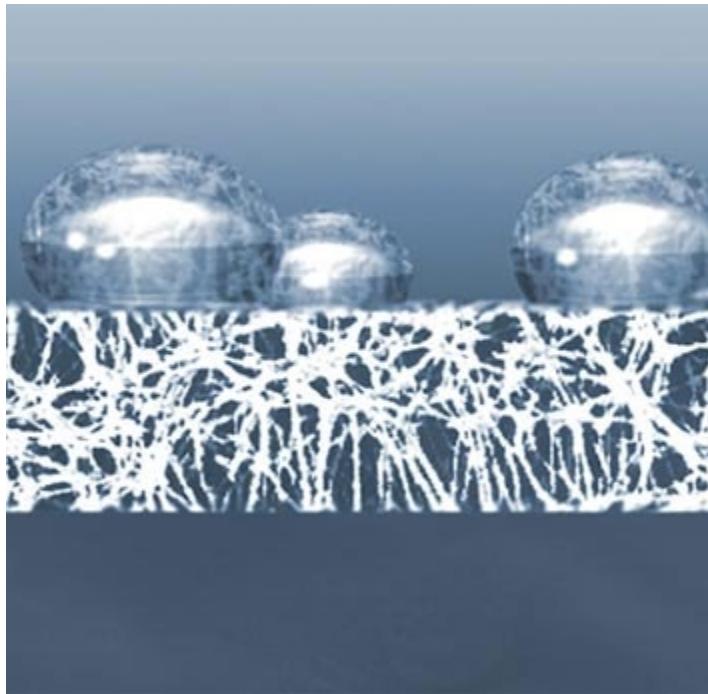
PDMAEMA

PMMA

PTBMA

Film – Surface Wetting

Water-proof, breathable textiles (Gore-Tex®)



„GORE-TEX® products are based on GORE-TEX® ePTFE membrane technology. The membrane provides a thin, uniform barrier that can provide properties like waterproofness or chemical resistance. A single square inch of the GORE-TEX® membrane contains 9 billion microscopic pores — each 20,000 times smaller than a raindrop but 700 times larger than a molecule of water vapor — so while water can't pass through the fabric, perspiration can. Integrated into the ePTFE structure is an oleophobic, or oil-hating, substance that allows moisture vapor to pass through but is a physical barrier that prevents the penetration of contaminating substances such as oils, cosmetics, insect repellents, and food substances“

Outline

- I: Introduction
- II: Wetting/Dewetting Contact Angle**
- III: Characterization of Surfaces

Contact Angle

Measuring static and dynamic contact angle

Contact angle hysteresis

Young equation – Droplet size

Critical surface tension – Zisman plot

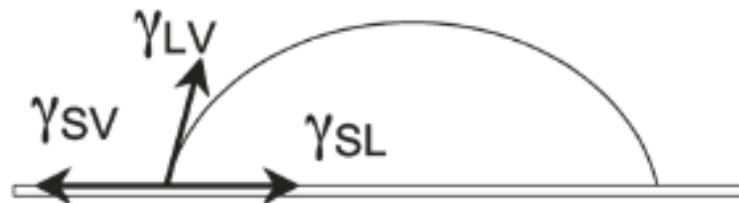
Surface roughness

Models of Wenzel and Cassie

Contact Angle

Contact Angle – A three face boundary

- liquid-vapor (LV)
- solid-liquid (SL)
- solid-vapor(SV)



Variables/Challenges:

- drop size & drop height
- surface morphology
- evaporation time vs. measurement
- temperature and humidity
- surface impurities

Contact Angle

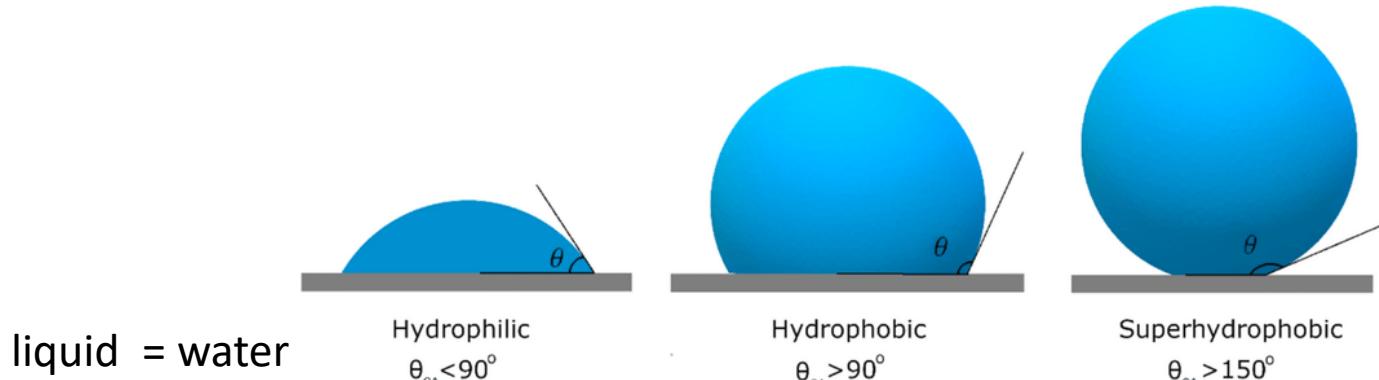


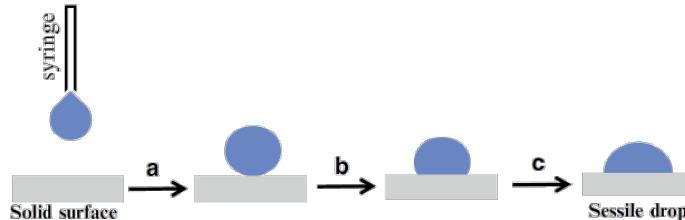
TABLE 3 Concerns in Contact Angle Measurement

- The measurement is operator dependent.
- Surface roughness influences the results.
- Surface heterogeneity influences the results.
- The liquids used are easily contaminated (typically reducing their ν_{lv}).
- The liquids used can reorient the surface structure.
- The liquids used can absorb into the surface, leading to swelling.
- The liquids used can dissolve the surface.
- Few sample geometries can be used.
- Information on surface structure must be inferred from the data obtained.

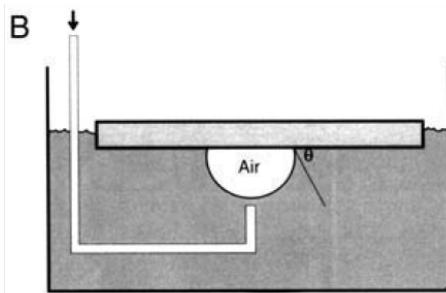
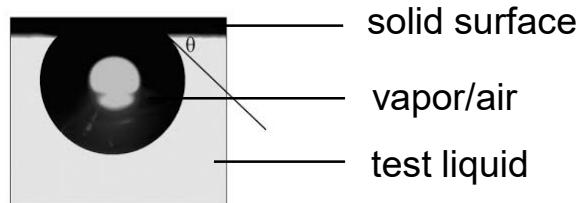
Static and Dynamic Contact Angle

static contact angle

- Sessile drop on a substrate

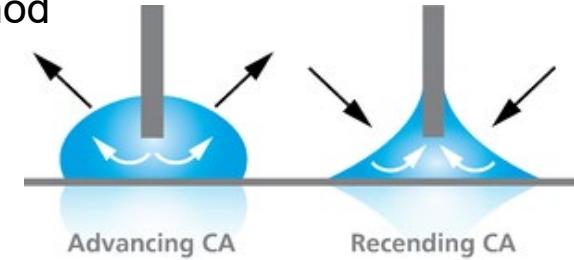


- captive bubble

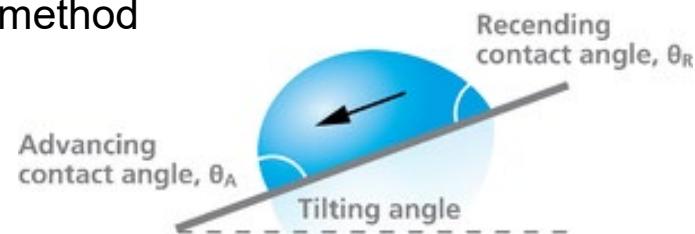


dynamic contact angle

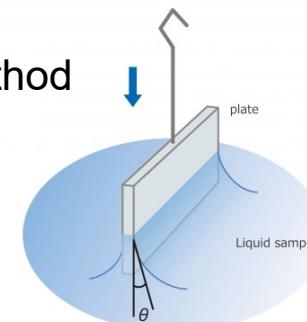
- needle method



- tilting method



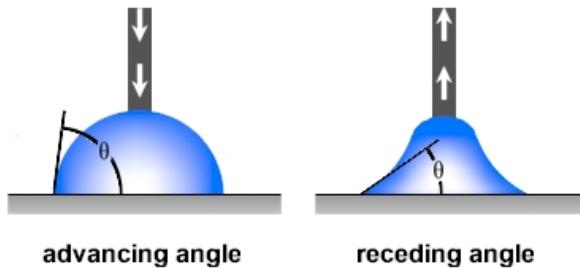
- Wilhelmy plate method



$$\gamma = \frac{F}{L \cos \theta}$$

Where:
 γ : Surface tension
 F : Measuring force (force acting on the plate)
 L : Perimeter of plate
 θ : Contact angle of plate and the liquid

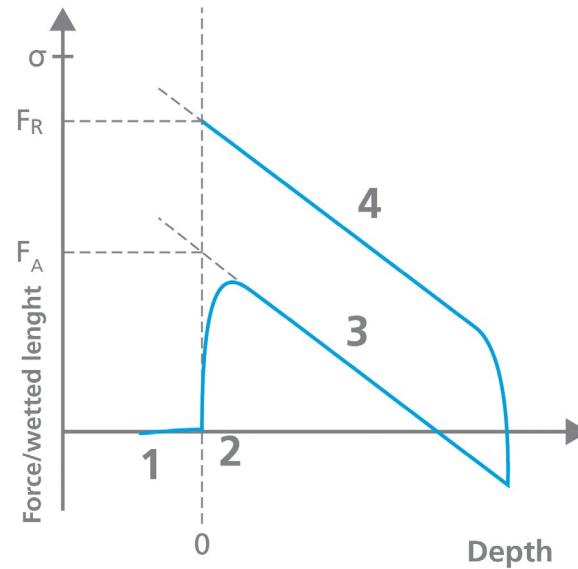
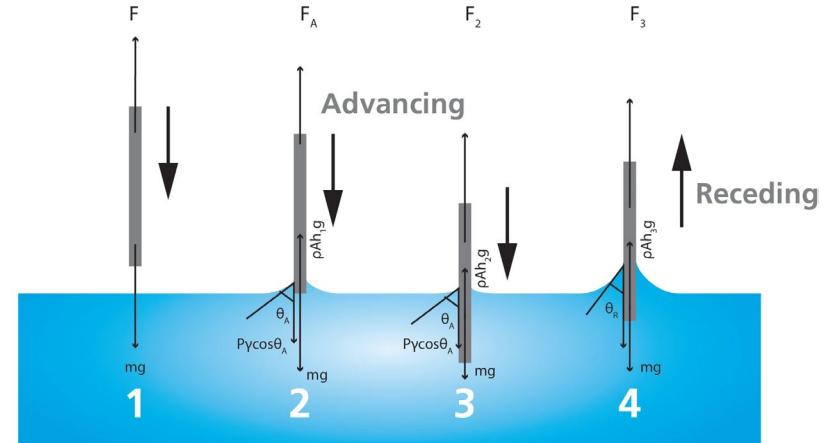
Contact Angle Hysteresis



In dynamic liquid systems, a liquid front advancing across a new surface may exhibit a large contact angle (the advancing contact angle θ_A), while the same liquid receding from an already wetted surface will have a much smaller contact angle (the receding contact angle θ_R). The difference between θ_A and θ_R is termed the contact angle hysteresis.

P is the perimeter of the plate,
 γ is the surface tension of the liquid,
 θ is the contact angle between the plate and the measured liquid,
 ρ is the density of the liquid,
A is the surface area of the plate,
h the immersion depth, and
g the gravitational constant.

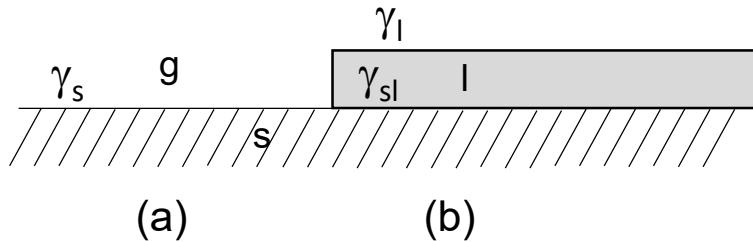
The first term on the right-hand side of the equation is caused by wetting force and the second by buoyancy.



$$F(h) = P\gamma\cos\theta - \rho Ahg$$

Spreading Coefficient

Spreading refers to movement of a phase front whereby the interfacial area is increased.



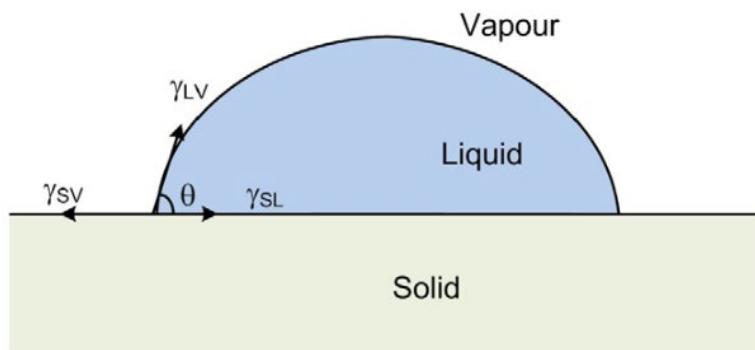
the surface free energy of (a) γ_s is per unit area and of (b) $\gamma_{sl} + \gamma_l$ where two interfaces are included. It is assumed that the spread liquid film is sufficiently thick such that the two interfaces are independent from each other (γ_l is of bulk liquid)

$$S = \lambda_{ls} = \gamma_s - \gamma_{sl} - \gamma_l$$

$S \geq 0$: liquid spreads completely – complete wetting

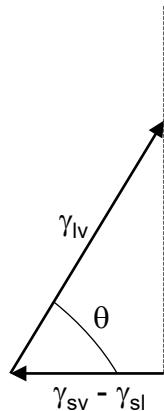
$S < 0$: no or partial wetting

Contact Angle Equilibrium: Young Equation



Stable equilibrium will be obtained if the solid surface is ideally smooth, homogenous, planar, and undeformable; the angle formed is the equilibrium contact angle.

$$\cos \theta = \frac{\gamma_{sv} - \gamma_{sl}}{\gamma_{lv}}$$

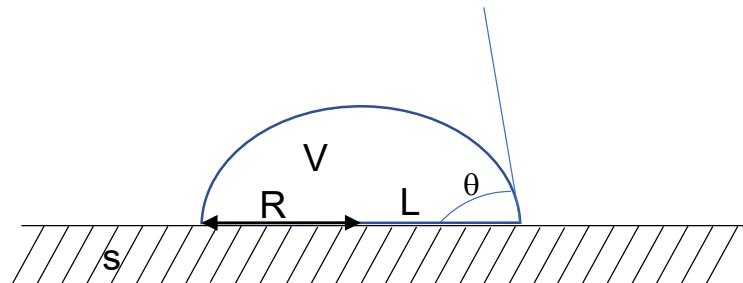


$$\gamma_{lv} \cos \theta = \gamma_{sv} - \gamma_{sl}$$

$\theta = 0^\circ$ complete wetting
 $\theta = 180^\circ$ complete dewetting

With spreading coefficient: $S = \gamma_{lv} (\cos \theta - 1)$

Forces in Droplets



Droplet of radius R with a volume V .
Contact line L is a circle with radius R .

Forces at equilibrium of partial wetting:

horizontal: Young equation $\gamma_{lv} \cos\theta = \gamma_{sv} - \gamma_{sl}$

and vertical : capillary forces on line L , Laplace pressure and gravity

$$\gamma \sin\theta$$

$$p_L \approx \frac{\gamma}{R}$$

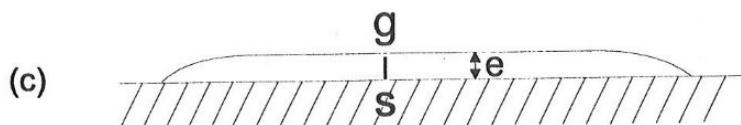
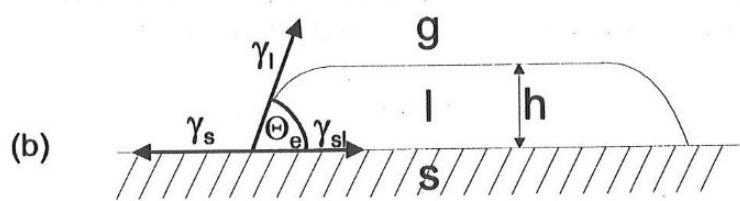
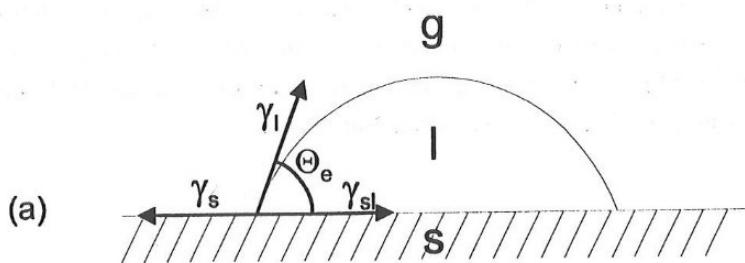
$$\rho gh$$

From Droplets to Film

force equilibrium: $\gamma_s = \gamma_{sl} + \gamma_l - \frac{1}{2} \rho g h^2$

capillary length (or capillary constant) k^{-1} :

$$k^{-1} = \left(\frac{\gamma_l}{\rho g}\right)^{1/2}$$



$$e \approx 10 - 100 \text{ \AA}$$

For small droplets the gravity can be neglected

$$R \ll k^{-1}$$

Droplets with increased volume are flatten by gravity resulting in a disc of height h

$$R \gg k^{-1}$$

Complete wetting $S \geq 0$, spreading occurs until a film of thickness e and surface A is formed.

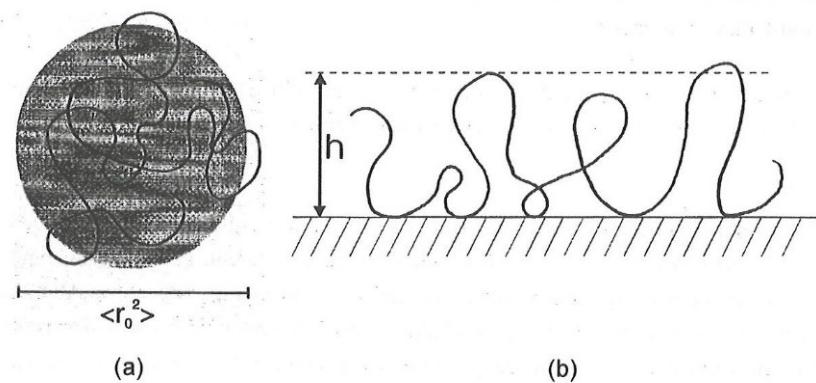
$$\text{free energy of spreading: } \Delta F = -SA + P(h)A$$

with S : spreading coefficient

$P(h)$: long range Van der Waals forces

Thickness of Polymer Films

A random coil of a polymer chain with N monomers is placed on a smooth, hard, solid surface



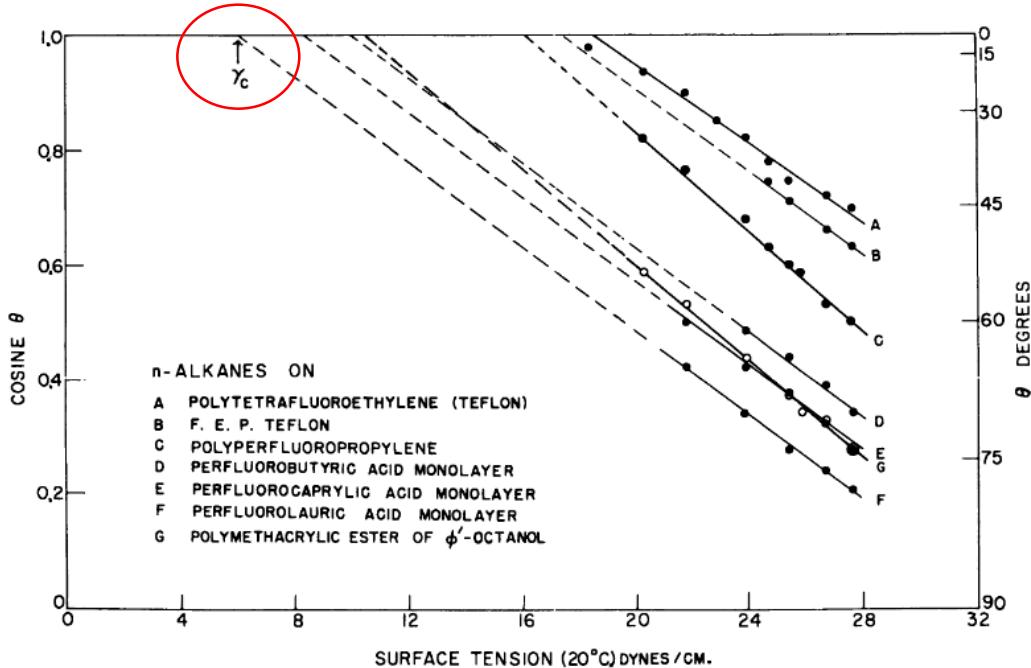
rms end-to-end distance
is greater than the
minimum film thickness e

film thickness is determined by the free surface energy F_s and
additionally by the deformation energy F_{def}

$$\Delta F = \Delta F_s + \Delta F_{\text{def}}$$

$$\Delta F_{\text{def}} \approx \alpha^{-2} + \ln \alpha^2 \quad \text{with } \alpha = \sqrt{\frac{h}{N}}$$

Critical Surface Tension – Zisman plot



Semi-empirical linear relation between contact angles of a series of homologous liquids on a surface to the surface tension of these liquids.

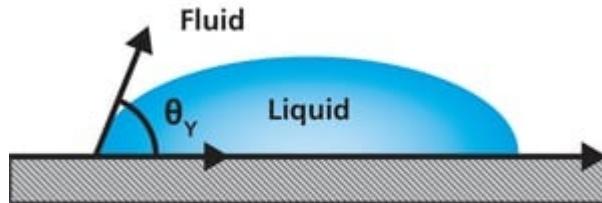
The critical surface tension γ_c is obtained by extrapolation to complete wetting ($\cos\theta = 1$).

$$\cos\theta = 1 + m(\gamma_l - \gamma_c)$$

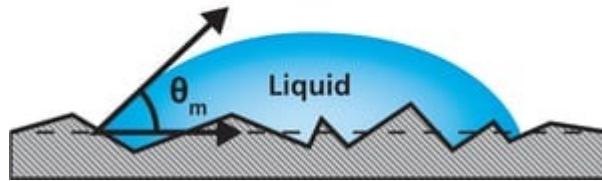
TABLE 17.1. Values of Critical Surface Tension of Wetting (σ_c , mN cm^{-1}) for Various Materials

Solid	σ_c	Solid	σ_c
Teflon	18	Copper	60
Polytrifluoroethylene	22	Silver	74
Polyvinylidene fluoride	25	Silica (dehydrated)	78
Polyvinyl fluoride	28	Anatase (TiO_2)	92
Polyethylene	31	Graphite	96
Polystyrene	33	Lead	99
Polyvinyl alcohol	37	Tin	101
Polyvinyl chloride	39	Iron	106
Polyvinylidene chloride	40	Iron oxide(Fe_2O_3)	107
Polyethyleneterephthalate	43	Silica (hydrated)	123
Nylon 6,6	46	Rutile (TiO_2)	143

Influence of Surface Roughness

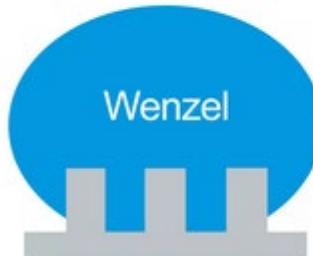


On the ideal surface, Young's equation applies, and the measured contact angle is equal to the Young's contact angle θ_Y



a real surface, the actual contact angle is the angle between the tangent to the liquid-fluid interface and the actual, local surface of the solid: θ_m

→ Models of Wenzel and Cassie/Baxter: a drop on a structured surface



Influence of Roughness on Wettability

$\Theta > 90^\circ$: Surface roughness increases the hydrophobic character of a non-wetting surface

$\Theta < 90^\circ$: Surface roughness improves the wettability of a hydrophilic surface

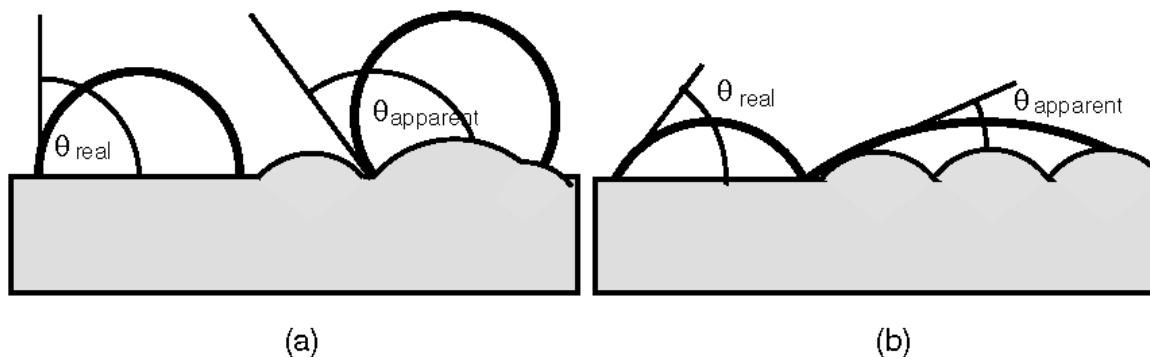


FIGURE 6.15. On a rough surface, the apparent contact angle can differ significantly from the “real” angle that would be observed on a molecularly smooth surface of the same material: (a) if the real contact angle is greater than 90°, the apparent angle will be even larger; (b) if the real angle is less than 90°, the apparent angle will be smaller.

Wenzel Model (1936)

$$\cos\theta^* = r \left(\frac{\gamma_{S2} - \gamma_{S1}}{\gamma_{12}} \right) = r \cos\theta_Y$$

with: $r = \frac{\text{real surface area}}{\text{projected flat surface area}}$

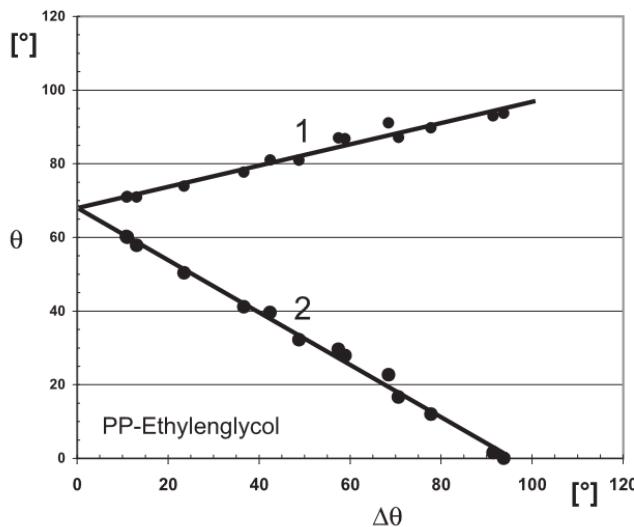
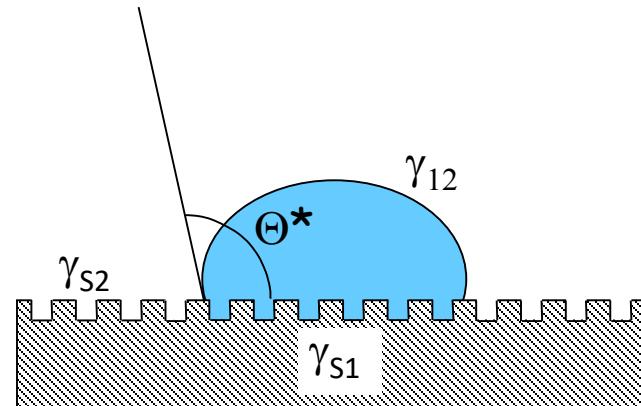


FIGURE 1 Advancing (1) and receding (2) contact angles measured with ethylene glycol on polypropylene samples with varying contact angle hysteresis due to varied roughness

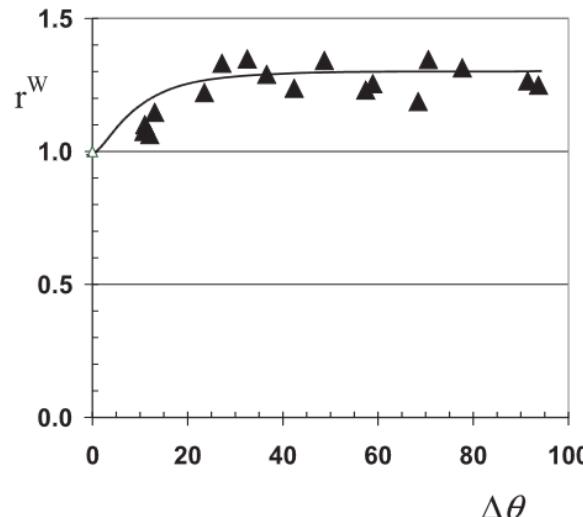
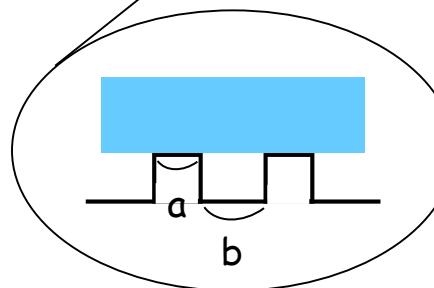
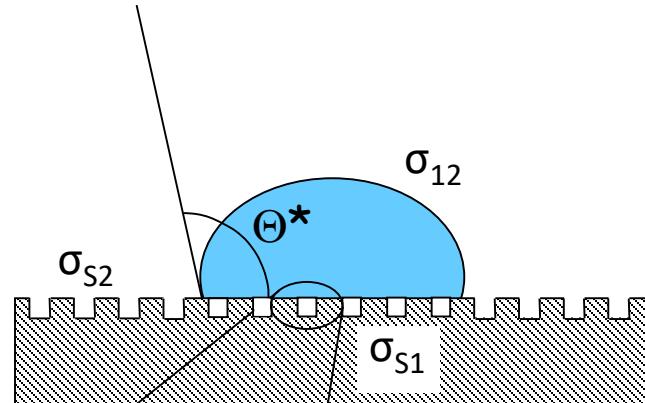


FIGURE 4 Roughness factor r^W , calculated by (11) from contact angle data, as a function of contact angle hysteresis $\Delta\theta$ for ethylene glycol on polypropylene for a series of samples varying roughness

Superhydrophobicity: Cassie – Baxter Model (1948)

This equation assumes a droplet on a porous surface where the pores are filled with air

$$\begin{aligned}\cos \Theta^* &= f \cos \Theta + (1 - f) \cos 180^\circ \\ &= f \cos \Theta - 1 + f \\ &= f (\cos \Theta + 1) - 1\end{aligned}$$



$$f = \frac{\sum a}{\sum(a + b)}$$

Where:

a = total area of solid – liquid interface

b = total area of liquid – air interface

Example Lotus Effect: Surface Structure and Wettability



Hierarchical surface structure

- Epidermal Cells
- Hydrophobic waxes crystals

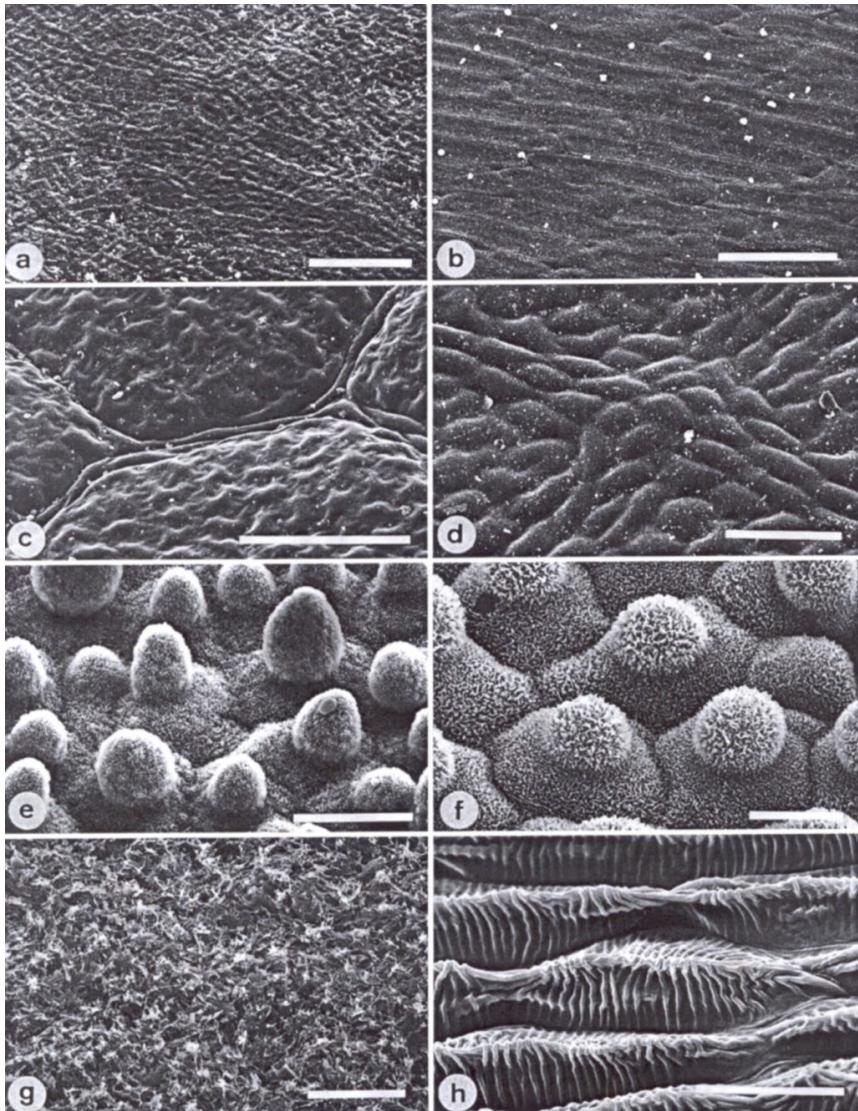


Table 1. Mean values (\pm SD) of 20 measurements of the static CA ($^\circ$) on the adaxial leaf surfaces of the species used for contamination experiments

Plant species	CA
b) <i>Heliconia densiflora</i>	28.4 ± 4.3
a) <i>Gnetum gnemon</i>	55.4 ± 2.7
d) <i>Magnolia denudata</i>	88.9 ± 6.9
c) <i>Fagus sylvatica</i>	71.7 ± 8.8
e) <i>Nelumbo nucifera</i>	160.4 ± 0.7
f) <i>Colocasia esculenta</i>	159.7 ± 1.4
g) <i>Brassica oleracea</i>	160.3 ± 0.8
h) <i>Mutisia decurrens</i>	128.4 ± 3.6

Fig. 1a-h. Scanning electron micrographs of the adaxial leaf surface of smooth, wettable (a-d) and rough, water-repellent (e-h) leaf surfaces. The smooth leaves of *Gnetum gnemon* (a) and *Heliconia densiflora* (b) are almost completely lacking microstructures while those of *Fagus sylvatica* (c) and *Magnolia denudata* (d) are characterized by sunken and raised nervature, respectively. The rough surfaces of *Nelumbo nucifera* (e) and *Colocasia esculenta* (f) are characterized by papillose epidermal cells and an additional layer of epicuticular waxes. *Brassica oleracea* leaves (g) are densely covered by wax crystalloids without being papillose, and the petal surfaces of *Mutisia decurrens* (h) are characterized by cuticular folds. Bars = 100 μ m (a-d) and 20 μ m (e-h)

The Wenzel Model versus the Cassie Model

Wenzel:

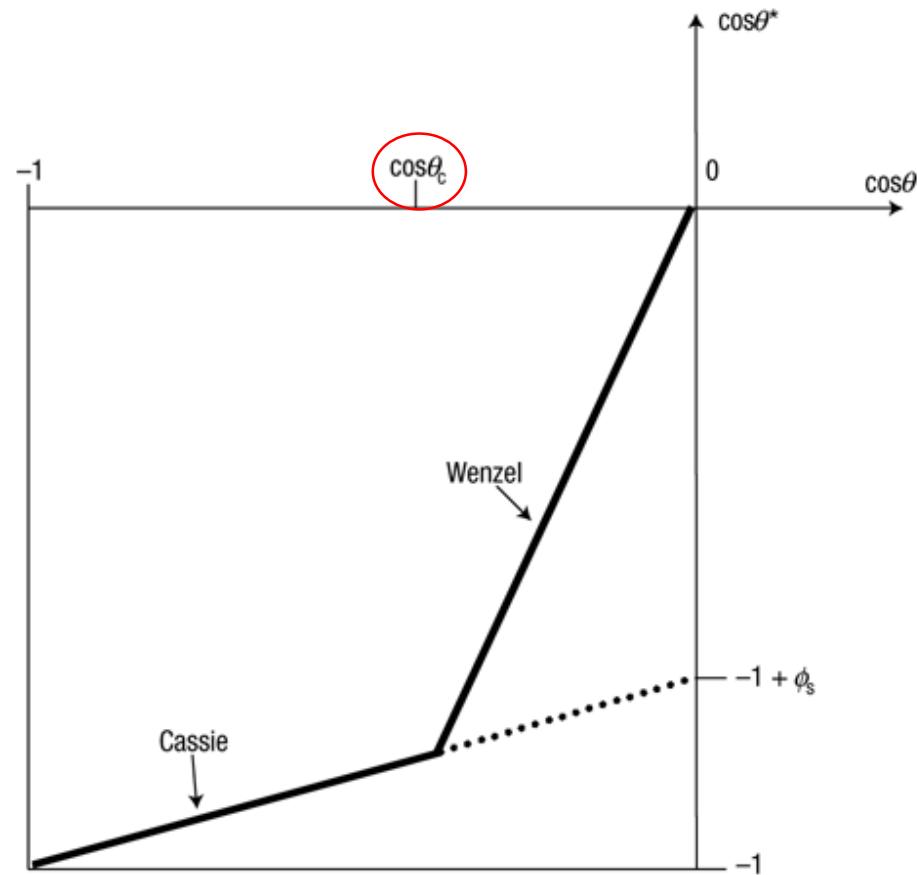
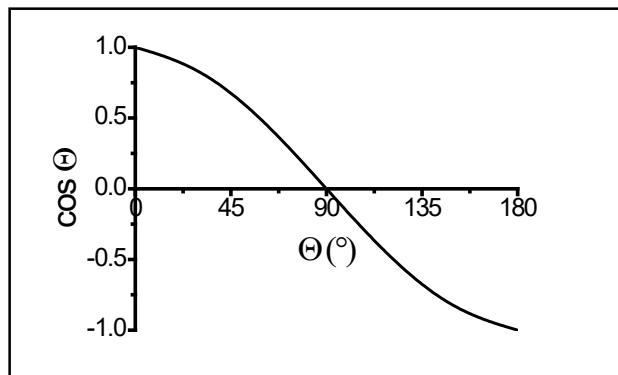
$$\cos \Theta^* = r \cos \Theta$$

Cassie:

$$\cos \Theta^* = f \cos \Theta - 1 + f$$

$$\cos \Theta_c = (f - 1)/(r - f)$$

threshold value between the two regimes



- Wenzel Regime: Moderately hydrophobic and rough surfaces
- Cassie Regime: Very hydrophobic and very rough surfaces (large Θ or r)

The Wenzel Model versus the Cassie Model

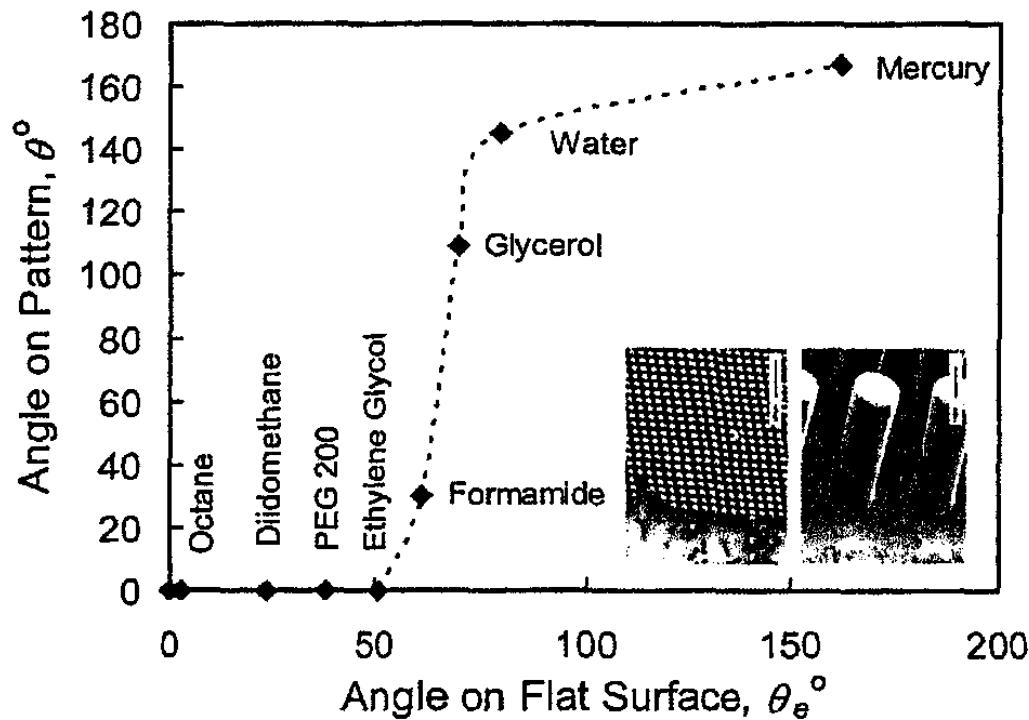
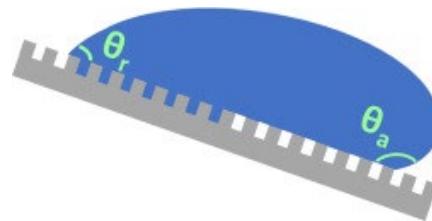
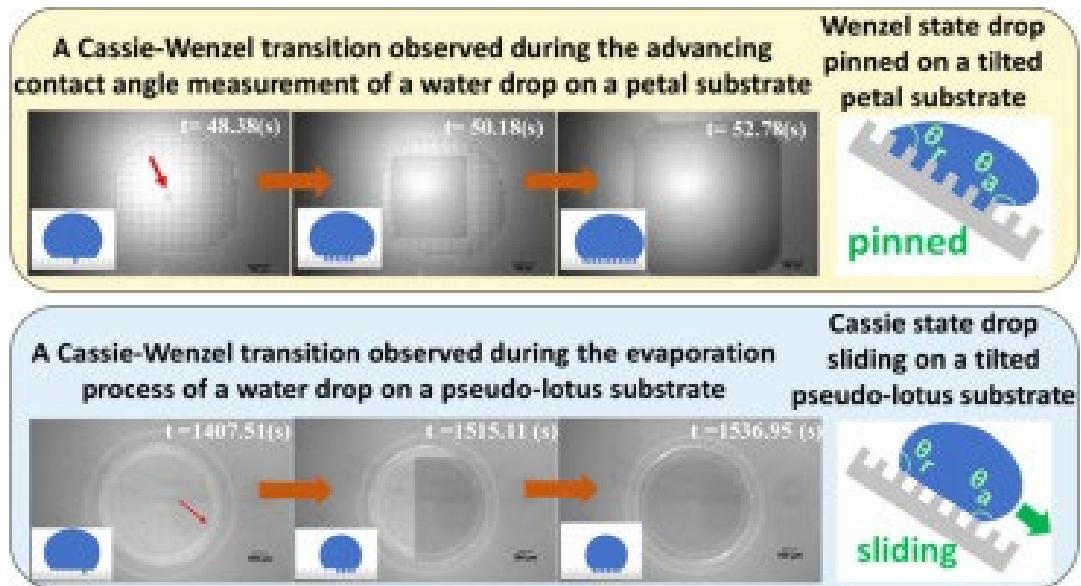


Fig. 2 Contact angles for a range of liquids on a textured SU-8 surface. The inset shows scanning electron microscope images of the lithographically structured surfaces showing a square lattice of 15 μm diameter cylindrical pillars with a 30 μm lattice parameter (view of a field of pillars and a close-up view of the pillars).

The Wenzel Model versus the Cassie Model



Schematic illustration of a water droplet in petal state on a single micro-scale roughness surface with a possible scenario that the front of the droplet, possessing ACA (θ_a), in Cassie state while the rear of the droplet, possessing RCA (θ_r), in Wenzel state.

